

Up-to-Date Finite Element Based Simulation of Permanent Magnet

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- Abstract: The paper presents a two dimensional finite element based solver for static magnetic field problems. The application has been written in C programming language. Magnetic vector potential of some reference models have been calculated by the help of two environments. The first one is the MATLAB environment and the second one is the C programming language based finite element code. The simulation results of the two environments were compared to each other focusing on the magnetic vector potential and the simulation time. Differences of the simulation results are showed in this paper, as well.
- Keywords: Finite Element Method, C programming language, MATLAB, permanent magnet

1. Introduction

The computer-aided design is one of the important parts of the electric engine development. Electric engines have been improved at the Széchenyi István University, as well and one of the parts of this development is to design and optimization a brushless DC (direct current) motor family, which are will be applied with bicycles and smaller motors. There are also two projects where these motors will be applied. One of them is the development of hybrid E-VAN, which is an adapted Ford-truck. The second one is an electric car which is an individual development by the students and teachers of the university. The main aspect of this PMS motor (Permanent Magnet Synchronous motor) development is to reduce the weight and the size of the engine but the torque and losses of the motor should not decrease. There are different ways to design the PMS motors. This paper shows a C programming language based finite element simulation of the permanent magnets which are used in permanent magnet synchronous motors.

2. Structure of the development environment

The new finite element package consists of two main parts which can be seen in Fig. 1. The first part is the GMSH software [1] which is a two and three-dimensional finite element mesh generator with built-in pre- and post-processing facilities. The second part of the finite element development environment is the C language based package under

Linux operating system, where partial differential equations and matrix operations can be solved. The finite element based solver has been written by the help of this package.



Figure 1. Structure of the development environment

Many data have to be used in the FEM (Finite Element Method) structure. For example number of nodes, number of elements, material parameters, etc., which are given from the geometry and the mesh in the pre-procession step? These parameters and data are used in the Analysis step to solve the equations of partial differential equations. And finally the data of the simulation results are shown in the post-procession step.

Fig. 2. shows the graphical user interface of the finite element based package which consists of two parts.



Figure 2. Graphical User Interface

On the left side the mesh, material parameters and boundary conditions can be set. And on the right side the model and the simulation results can be seen which a permanent magnet is.

3. Governing Equations

The basic model consists of a permanent magnet, a ferrite core and an excited single coil which can be seen in Fig. 3.



Figure 3. Scheme of the basic model

From the basic model five simple different arrangements had been created. The different simulated arrangements are as follows:

- One turned excited coil;
- One turned excited coil with ferrite core;
- Permanent magnet;
- Permanent magnet with ferrite core;
- The basic model which contains the permanent magnet, the ferrite core and the excited coil, as well.

These models have been calculated in the C programing language based the finite element environment and in MATLAB environment.

The simulated problem has been modelled as a static magnetic field problem, where the following Maxwell's equations can be used [2]-[5]:

$$\nabla \times \boldsymbol{H} = \boldsymbol{J}_0, \text{ in } \Omega_0 \cup \Omega_{\mathrm{m}}, \tag{1}$$

$$\nabla \cdot \boldsymbol{B} = 0, \text{ in } \Omega_0 \cup \Omega_{\text{m}}. \tag{2}$$

Here H is the magnetic field intensity, J_0 is the source current density, B is the magnetic flux density. The H magnetic field intensity can be expressed as

$$\boldsymbol{H} = \begin{cases} \nu_0 \boldsymbol{B}, \text{ in } \Omega_0 \\ \nu_0 \nu_r \boldsymbol{B} \text{ in } \Omega_m \end{cases}$$
(3)

Here ν_0 is the reluctivity of vacuum and ν_r is the relative reluctivity of magnet. The air region is denoted by Ω_0 and the magnetic region is denoted by Ω_m . The *A* magnetic flux density can be expressed as

$$\boldsymbol{B} = \nabla \times \boldsymbol{A},\tag{4}$$

where *A* is the magnetic vector potential [2]-[5]. This expression satisfies (2), because of the identity $\nabla \cdot \nabla \times \boldsymbol{v}$ for any vector function $\boldsymbol{v} = \boldsymbol{v}(\boldsymbol{r})$.

When the domain contains permanent magnets, their magnetic characteristic are given by [3]

$$\boldsymbol{B} = \boldsymbol{\mu}\boldsymbol{H} + \boldsymbol{B}_0,\tag{5}$$

where B_0 is the remanent flux density. Substituting (1) and (4) to (5) and using the constitutive relations IS (3) the following partial differential equation can be obtained:

$$\nabla \times \frac{1}{\mu} \nabla \times \boldsymbol{A} - \nabla \times \frac{1}{\mu} \boldsymbol{B}_0 = \boldsymbol{J}_0.$$
(6)

The divergence of the magnetic vector potential can be selected according to Coulomb's gauge [5,7],

$$\nabla \cdot \boldsymbol{A} = 0$$

which is satisfied automatically in two dimensional problems [4], [5]. Using some mathematical identity and using some formulations [4], [5], the following weak equation can be obtained

$$\int_{\Omega} \frac{1}{\mu} \nabla \times \boldsymbol{W} \cdot \nabla \times \boldsymbol{A} \, \mathrm{d}\Omega - \int_{\Omega} \frac{1}{\mu} \nabla \times \boldsymbol{W} \cdot \boldsymbol{B}_{0} \, \mathrm{d}\Omega = \int_{\Omega} \boldsymbol{W} \cdot \boldsymbol{J}_{0} \, \mathrm{d}\Omega \,, \tag{7}$$

which solution results in the approximation of the magnetic vector potential.

4. Simulation results of the models

Five simple different arrangements had been created from the basic model. These models are calculated in the C programing language based on the finite element environment and in MATLAB environment. The simulation results were compared each other focusing the time and the accurate of the magnetic vector potential. In both environments the unknowns are the same, or closely the same which is 12790.

4.1. Comparison of the computation time of the models

Computation times of two different development environment are compared with each other. The sum up of the computation times of the simulations can be seen in Table 1.

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model	MATLAB	С
excited coil	60sec	13sec
ferrite core and excited coil	60sec	13sec
magnet	60sec	12sec
magnet and ferrite core	59sec	10sec
magnet, ferrite core and excited coil	63sec	11sec

Table 1. Computation times of models in two different environments

On the left side the computation times in MATLAB environment are shown, and on the right side the computation times in C environment are shown in Table 1. In case of every arrangement the problem was calculated almost five times faster by the help of the C environment than with MATLAB.

4.2. Comparison of the magnetic vector potential of the models

Simulation results were also compared with each other focusing on the accuracy of the magnetic vector potential. Fig. 4. shows the simulation result of the magnetic potential in the case of excited one turned coil model. Fig 4a shows the simulation results in GMSH environment. Fig. 4b shows the simulation results in MATLAB environment.



Figure 4. Simulation results of excited coil

Comparing Fig. 4a and 4b, it can be seen that the magnitude of the magnetic vector potential in the model are similar.

Fig. 5. shows the simulation result of the magnetic potential, where the model consists an excited one turned coil with ferrite core. Fig. 5a shows the simulation results in GMSH environment. Fig. 5b shows the simulation results in MATLAB environment.



Figure 5. Simulation results of excited coil with ferrite core

Comparing the Fig. 5a and 5b figures with each other, it can be seen that the magnitude of the magnetic vector potential in the model are similar.

Fig. 6. shows the simulation result of the magnetic potential, where the model consists a permanent magnet. Fig. 6a shows the simulation results in GMSH environment. Fig. 6b shows the simulation results in MATLAB environment.



Figure 6. Simulation results of magnet

Comparing the Fig. 6a and 6b figures with each other, it can be seen that the magnitude of the magnetic vector potential in the model are similar.

Fig. 7. shows the simulation result of the magnetic potential, where the model consists a permanent magnet with ferrite core. Fig. 7a shows the simulation results in GMSH environment. Fig. 7b shows the simulation results in MATLAB environment.



Figure 7. Simulation results of magnet with ferrite core

Comparing the Fig. 7a and 7b, it can be seen that the magnitude of the magnetic vector potential in the model are similar.

Fig. 8. shows the simulation result of the magnetic potential, where the model consists of a permanent magnet with ferrite core and one turned excited coil. Fig. 8a shows the simulation results in GMSH environment. Fig. 8b shows the simulation results in MATLAB environment.



Figure 8. Simulation results of magnet, ferrite core and excited coil

Comparing the Fig. 8a and 8b, it can be seen that the magnitude of the magnetic vector potential in the model are similar.

4.3. Differences of the simulation results

Simulation results were also compared with each other focusing on the magnitude of the differences of models.

Fig. 9. shows the differences of the simulation results of the two different development environment in the case of the model of one turned excited coil.



Figure 9. Margin between the simulation results, model: excited coil

The magnitude of the difference of the simulation results is about 10^{-5} .

Fig. 10. shows the differences of the simulation results of the two different development environment in the case of the model of one turned excited coil with ferrite core.



Figure 10. Margin between the simulation results, model: excited coil with ferrite core

The magnitude of the difference of the simulation results is about 10^{-4} .

Fig. 11. shows the differences of the simulation results of the two different development environment in the case of the model of permanent magnet.



Figure 11. Margin between the simulation results, model: magnet

The magnitude of the difference of the simulation results is about 10^{-4} .

Fig. 12. shows the differences of the simulation results of the two different development environment in the case of the model of permanent magnet with ferrite core.



Figure 12. Margin between the simulation results, model: magnet with ferrite core

The magnitude of the difference of the simulation results is about 10^{-4} .

Fig. 13. shows the differences of the simulation results of the two different development environment in the case of the model of permanent magnet with ferrite core and one turned excited coil.



Figure 13. Margin between the simulation results, model: magnet, ferrite core and excited coil

The magnitude of the difference of the simulation results is about 10^{-4} . It can be seen in every case that the differences of the simulation results are very small.

5. Conclusion

The new, finite element package based on C programming language is faster than the MATLAB solver, but the accuracy of the simulation results is adequate.

In the future work this C programming language based finite element package will be used for simulation and optimization of permanent magnet synchronous motors in a more fast and accurate way. This solution will have used in a research work where arrangements of the magnets and air gaps of the rotor of the BLDC motor to develop more energy efficient BLDC motors will have investigated.

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